

To: Derek Lyman, Highway Safety and Design, Project Manager
MLM CCB

From: Marcy Meyers, Geotechnical Engineer, via Christopher C. Benda P.E., Soils and Foundations Engineer

Date: October 24th, 2013

Subject: Williston STP-HES 5500(12) – Geotechnical Data Report

1.0 INTRODUCTION

We have completed our geotechnical investigation for the Williston STP-HES 5500(12) project located along VT Route 2A beginning approximately 500 feet south of River Cove Road and extending northerly to approximately 600 feet north of East View Circle in the Town of Williston, Vermont. The proposed project consists of roadway rehabilitation including intersection improvements as well as the installation of two mast arms. This report summarizes the boring and laboratory testing information from our subsurface investigation and contains geotechnical parameters to be used by the mast arm foundation designer.

2.0 FIELD INVESTIGATION

The initial field investigation was conducted between August 29th and September 4th, 2013. Two standard penetration borings and eleven solid stem auger roadway borings were drilled to determine the soil strata for the proposed project. An additional boring, B-102A, was drilled on October 10th, 2013 in order to collect undisturbed Shelby tube samples for testing of cohesive material found in the initial investigation. Final boring locations were provided in an email by Erik Atkins dated July 30th, 2013. Values for Northings, Eastings, and elevations were provided on the Williston boring and pavement core plan and modified when applicable. The values for Northings and Eastings are based on the Vermont State Plane Grid NAD 83 coordinate system. Boring location information is summarized below in Table 2.1.

Table 2.1: Boring Locations

| Boring | Drilling Method | Station (ft) | Offset (ft) | Approx. Northing (ft) | Approx. Easting (ft) | Approx. Elevation (ft) |
|--------|-----------------|--------------|-------------|-----------------------|----------------------|------------------------|
| B-101 | WB/SPT | 98+50.02 | -36.0 | 720634.01 | 1480274.48 | 358.47 |
| B-102 | WB/SPT | 98+91.32 | 30.2 | 720677.02 | 1480342.49 | 355.22 |
| B-102A | WB/UD | 98+91.30 | 31.0 | -- | -- | -- |
| PC-1 | SSA | 85+14.18 | 7.5 | 719299.88 | 1480355.90 | 395.85 |
| PC-2 | SSA | 85+14.18 | -7.7 | 719299.24 | 1480340.69 | 395.75 |
| PC-3 | SSA | 90+6.66 | 7.7 | 719792.21 | 1480343.21 | 384.54 |
| PC-4 | SSA | 90+6.66 | -7.7 | 719791.54 | 1480327.79 | 384.46 |
| PC-5 | SSA | 94+61.52 | 6.3 | 720246.91 | 1480329.89 | 371.48 |
| PC-6 | SSA | 94+61.52 | -7.5 | 720246.24 | 1480316.10 | 371.62 |
| PC-7 | SSA | 100+6.66 | 8.0 | 720791.86 | 1480317.30 | 353.93 |
| PC-8 | SSA | 100+6.66 | -8.2 | 720791.30 | 1480301.15 | 354.11 |
| PC-9 | SSA | 105+75.18 | 9.3 | 721360.41 | 1480293.58 | 333.43 |

| | | | | | | |
|-------|-----|-----------|-------|-----------|------------|--------|
| PC-10 | SSA | 105+75.18 | -9.3 | 721358.09 | 1480275.08 | 332.73 |
| PC-11 | SSA | 31+7.72 | -10.0 | 720645.07 | 1480205.47 | 355.56 |

SSA = Solid Stem Auger, WB = Wash Bore, SPT = Standard Penetration Test, UD = Undisturbed Shelby Tubes

Borings B-101, B-102, and B-102A were performed in general accordance with AASHTO T206, *Standard Method of Test for Penetration Test and Split-Barrel Sampling of Soils*. During boring operations, split spoon samples and standard penetration tests (SPT) were taken continuously from 2'-12' and then 5' intervals to a depth of approximately 25' for Borings B-101 and B-102.

The solid stem auger borings were performed in general accordance with AASHTO T306, *Processing Auger Borings for Geotechnical Explorations*, to determine the subsurface profile to aid in the design and reconstruction of VT Route 2A and James Brown Drive. A 4-inch solid stem auger flight was rotary drilled to 5 feet below the top of the roadway for the 11 roadway borings. The auger was then removed so that a visual observation of the soil profile could be made. This method has proven to be an efficient and reasonably accurate way to view changes in strata and obtain samples off the auger flights.

Soil samples were visually identified in the field and SPT blow counts were recorded on the boring logs when applicable. Soil samples were preserved and returned to the Materials and Research laboratory for testing and further evaluation. Upon completion of the laboratory testing, the boring logs were revised to reflect the results of the laboratory classification results.

3.0 FIELD AND LABORATORY TESTS

The standard penetration resistance of the in-situ soil is determined by the number of blows required to drive a 2 inch OD split barrel sampler into the soil with a 140 pound hammer dropped from a height of 30 inches, in accordance with procedures specified in AASHTO T206. During the standard penetration test (SPT), the sampler is driven for a total length of 2 feet, while counting the blows for each 6 inch increment. The SPT N-value, which is defined as the sum of the number of blows required to drive the sampler through the second and third increments, is commonly used with established correlations to estimate a number of soil parameters, particularly the shear strength and density of cohesionless soils. The N-values provided on the boring logs are raw values and have not been corrected for energy, borehole diameter, rod length, or overburden pressure. The VT Agency of Transportation has determined a hammer correction value, C_E , to account for the efficiency of the SPT hammer on the drill rig. For this project, a CME 45C track rig was used, with a $C_E=1.34$. This value, included on the boring logs, was used in soil parameter calculations. Laboratory tests were conducted on all samples to evaluate grain size, moisture content, percent finer than No. 200 sieve, and liquid and plastic limits when applicable.

When cohesive soils were encountered, undisturbed sampling was performed in accordance with AASHTO T207, *Thin Walled Tube Sampling of Soils*. A total of three Unconfined Compression Tests were performed on the undisturbed samples from B-102A in accordance with AASHTO T208, *Standard Method of Test for Unconfined Compressive Strength of Cohesive Soil*. This test provides the unconfined compressive strength (q_u) for a cohesive soil sample that can be used to determine the undrained shear strength (s_u) of the soil. The sample is loaded axially, without any confining pressures, at a relatively high rate to prevent drainage until a shear failure is reached.

The magnitude of the shear stress at the moment of failure results in the shear strength of the soil provided similar in-situ loading and drainage conditions. Results from this testing are attached.

In addition to pushing undisturbed Shelby tube samples, field vane shear testing was performed in Boring B-102A in accordance with AASHTO T223, *Standard Method of Test for Field Vane Shear Test in Cohesive Soil*. The torque required to turn the vane can be correlated to determine the undrained shear strength of the soil. The results of the vane shear testing can be found on the attached boring logs.

4.0 SOIL PROFILE

Review of the laboratory data, and boring logs revealed the following information pertaining to the soil strata. It should be noted that groundwater elevations are subject to change given the fact that the boreholes were generally left open for a short period of time and groundwater readings were collected during the same day as drilling. Because groundwater elevations can fluctuate seasonally and are effected by temperature and precipitation, groundwater may be encountered during construction even when not previously noted on the boring logs.

4.1 Roadway Auger Borings (PC-1 through PC-11)

The thickness of the bituminous pavement varied from 0.32 to 1.19 feet thick. The pavement overlies a layer comprised of silty sand with some gravel mixed throughout. PC-10 had some clay evident in the sample and was the only sample deemed plastic. All other samples were deemed non-plastic and groundwater was not encountered during drilling in any of the samples.

The attached drilling notes contain specific information regarding particle percentages, depths, and additional tests, if applicable. Also attached is a visual representation of the subsurface profile, interpreted by the borings, showing the various strata.

4.2 Mast Arm Borings (B-101 and B-102)

4.2.1 B-101: The ground surface elevation at B-101 was 358.47 feet. Groundwater was recorded at a depth of 6.0 feet below the ground surface while drilling. This results in an approximate groundwater elevation of 352.47 feet.

| Depth (Below Ground Surface Elevation) | Soil Profile |
|--|--------------------------------|
| 0.0 – 4.0 feet | Loose Gravelly Silty Sand |
| 4.0 – 6.0 feet | Medium Dense Silt |
| 6.0 – 20.0 feet | Very Stiff Silty Clay |
| 20.0 – 26.4 feet | Very Dense Gravelly Sandy Silt |

4.2.2 B-102: The ground surface elevation at B-102 was 355.22 feet. Groundwater was encountered at a depth of 1.6 feet below the ground surface during drilling operations and at the ground surface after drilling was complete. B-102A drilled only 0.8 ft away, encountered groundwater at a depth of 0.5 feet below the ground surface during drilling operations. As a result, an approximate groundwater elevation at the ground surface was used in soil parameter calculations.

| Depth (Below Ground Surface Elevation) | Soil Profile |
|--|-------------------------|
| 0.0 – 2.0 feet | Soft Silty Clay |
| 2.0 – 2.4 feet | Medium Dense Silty Sand |
| 2.4 – 11.0 feet | Very Stiff Clay |
| 11.0 – 26.9 feet | Very Dense Till |

5.0 RECOMMENDATIONS

5.1 Design Guidelines

The Materials and Research Section of VTrans has developed *Materials and Research Engineering Instructions (MREI) 10-01*, which “standardizes VTrans’ foundation designs for overhead structures such as signals or sign bridges, mast arms, and strain poles during plan (preliminary and final) development or construction.” This document should be referenced for the contractor’s use and is available on the Agency’s website at the following address:

http://vtransengineering.vermont.gov/sites/aot_program_development/files/documents/materialsandresearch/MandRSoilEI - Overhead Structures 030910.pdf

5.2 Design Parameters

Laboratory results from the unconfined compression tests can be found in Table 5.1 and are also attached. Based on the soil profiles above, laboratory testing, and attached boring logs, the in-situ soil properties can be found in Table 5.2. Engineering values for common construction materials can be found in Table 5.3. These values presented in Tables 5.2 and 5.3 should be used in the design of the mast arm foundations at this location.

The boreholes were generally only open for a short period of time during drilling and clean-up activities. In addition, the soils at the site have a high fines content and produce water slowly. Since groundwater elevations can fluctuate seasonally and are effected by temperature and precipitation, a groundwater level at the ground surface is recommended for design.

Table 5.1. Unconfined Compression Test

| Boring | Depth Below Ground Surface Elevation (ft) | Undrained Shear Strength (s_u) in (psi) | Unconfined Compressive Strength (q_u) in (psi) |
|---------------------------|---|---|--|
| B-102A (V. Stiff Clay) | 2.4 – 11.0 | 23-36 | 47-73 |

The tables below highlight the geotechnical design parameters of the in-situ soils as well as regularly specified aggregates. These values should be used when designing any substructure units. It is recommended that values of K_0 be used for calculating earth pressures where the structure is not allowed to deflect longitudinally, away from or into the retained soil mass. Values for K_a should be utilized for an active earth pressure condition where the structure is moving away from the soil mass and K_p where the structure is moving toward the soil mass. K_a and K_p values are based on a vertical back of wall and a horizontal ground surface behind the wall.

Table 5.2. Engineering Properties of In-Situ Soils

| | Soft Silty Clay | Medium Dense Silty Sand/Silt | Very Stiff Clay/Silty Clay | Loose Gravelly Silty Sand | Very Dense Gravelly Sandy Silt/Till |
|---|------------------------|-------------------------------------|-----------------------------------|----------------------------------|--|
| Density, γ (lbs/ft ³): | 95 | 110 | 115 | 110 | 125 |
| Internal Friction Angle, ϕ (degrees) | 33 | 34 | -- | 31 | 36 |
| Soil Modulus, k (lb/in ³) | 30 | 60 | 400 | 25 | 125 |
| Undrained Shear Strength, s_u (lb/in ²) | -- | -- | 23 | -- | -- |
| Coefficient of Friction, f | | | | | |
| - mass concrete cast against soil: | 0.31 | 0.34 | 0.34 | 0.55 | 0.50 |
| - soil against precast/formed concrete: | 0.25 | 0.25 | 0.31 | 0.40 | 0.38 |
| Active Earth Pressure Coef., K_a : | 0.295 | 0.283 | 0.307 | 0.320 | 0.260 |
| Passive Earth Pressure Coef., K_p : | 3.392 | 3.537 | 3.255 | 3.124 | 3.852 |
| At-Rest Earth Pressure Coef., K_o : | 0.455 | 0.441 | 0.470 | 0.485 | 0.412 |

Table 5.3. Engineering Properties of Construction Materials

| | 703.01A - Granular Borrow | 704.08 - Granular Backfill for Structures |
|---|----------------------------------|--|
| Density (lb/ft ³): | 130 | 140 |
| Internal Friction Angle, ϕ (degrees) | 32 | 34 |
| Coefficient of Friction, f | | |
| - mass concrete cast against soil: | 0.45 | 0.55 |
| - soil against precast/formed concrete | 0.40 | 0.48 |
| Active Earth Pressure Coefficient, K_a : | 0.31 | 0.28 |
| Passive Earth Pressure Coefficient, K_p : | 3.25 | 3.54 |
| At-Rest Earth Pressure Coefficient, K_o : | 0.47 | 0.44 |

6.0 CONCLUSION

We recommend this report be included with the contract documents when the project is advertised.

Please feel free to contact us at (802) 828-2561 if you have any questions, or you would like to further discuss this report. Typed boring logs are attached and are available in the CADD design files:

M:\Projects\12D196\Materials&Research

Attachments: Boring Logs (3 Pages)
Drilling Notes (3 Pages)
Roadway Boring Profile Sheet (1 Page)
Unconfined Compression Test Lab Results (6 Pages)

cc: Erik Atkins, Green International Affiliates, Inc.
Read File/WEA
Project File/CCB
MLM

G:\Soils and Foundations\Projects\Williston STP-HES 5500(12)\REPORTS\Williston STP-HES 5500(12)
Geotechnical Data Report.doc



STATE OF VERMONT
 AGENCY OF TRANSPORTATION
 MATERIALS & RESEARCH SECTION
 SUBSURFACE INFORMATION

BORING LOG

WILLISTON
STP-HES 5500(12)
VT-2A ROADWAY

Boring No.: **B-101**
 Page No.: **1 of 1**
 Pin No.: **12D196**
 Checked By: **MLM**

Boring Crew: JUDKINS, DAIGNEAULT, HALL
 Date Started: 8/30/13 Date Finished: 8/30/13
 VTSPG NAD83: N 720634.01 ft E 1480274.48 ft
 Station: 98+50.02 Offset: -36.00
 Ground Elevation: 358.47 ft

Casing: WB Sampler: SS
 Type: WB I.D.: 4 in 1.5 in
 Hammer Wt: N.A. 140 lb.
 Hammer Fall: N.A. 30 in.
 Hammer/Rod Type: Auto/AWJ
 Rig: CME 45C TRACK $C_e = 1.34$

| Groundwater Observations | | |
|--------------------------|------------|-----------------|
| Date | Depth (ft) | Notes |
| 08/30/13 | 6.0 | While drilling. |
| | | |
| | | |

| Depth (ft) | Strata (1) | CLASSIFICATION OF MATERIALS (Description) | Blows/6" (N Value) | Moisture Content % | Gravel % | Sand % | Fines % | LL % | PI % |
|---|------------|---|--------------------|--------------------|----------|--------|---------|------|------|
| 5 | | A-2-4, GrSa, Dk/brn, Moist, Rec. = 0.8 ft | 1-2-1-4 (3) | 14.1 | 27.8 | 54.2 | 18.0 | | |
| | | A-2-4, SiSa, Dk/brn, MTW, Rec. = 1.2 ft | 2-3-3-2 (6) | 21.8 | 16.3 | 62.6 | 21.1 | | |
| | | A-4, Si, brn-gry, Wet, Rec. = 1.4 ft | 2-3-5-5 (8) | 24.6 | 5.6 | 19.0 | 75.4 | | |
| | | A-6, SiCl, brn-gry, MTW, Rec. = 1.8 ft | 4-5-5-6 (10) | 25.7 | 0.6 | 9.3 | 90.1 | 32 | 12 |
| | | A-4, ClSi, brn-gry, MTW, Rec. = 1.9 ft | 3-5-8-7 (13) | 26.5 | 7.8 | 6.6 | 85.6 | 29 | 8 |
| 10 | | A-6, SiCl, brn-gry, MTW, Rec. = 1.5 ft | 3-5-5-10 (10) | 26.9 | 0.8 | 3.9 | 95.3 | 37 | 15 |
| 15 | | Field Note:, No Recovery | 4-8-8-8 (16) | | | | | | |
| 20 | | A-4, GrSaSi, gry, Wet, Rec. = 0.5 ft | 10-22-25-25 (47) | 22.0 | 26.5 | 29.2 | 44.3 | | |
| 25 | | A-4, GrSaSi, gry, Moist, Rec. = 1.0 ft | 19-26-R@5.0" (R) | 10.2 | 21.9 | 24.6 | 53.5 | | |
| Hole stopped @ 26.4 ft | | | | | | | | | |
| Remarks: 1. Hole collapsed at 24.5 ft. | | | | | | | | | |

BORING LOG 2 WILLISTON STP-HES5500(12).GPJ VERMONT AOT.GDT 10/29/13

Notes:
 1. Stratification lines represent approximate boundary between material types. Transition may be gradual.
 2. N Values have not been corrected for hammer energy. C_e is the hammer energy correction factor.
 3. Water level readings have been made at times and under conditions stated. Fluctuations may occur due to other factors than those present at the time measurements were made.



STATE OF VERMONT
AGENCY OF TRANSPORTATION
MATERIALS & RESEARCH SECTION
SUBSURFACE INFORMATION

BORING LOG

WILLISTON
STP-HES 5500(12)
VT-2A ROADWAY

Boring No.: B-102
Page No.: 1 of 1
Pin No.: 12D196
Checked By: MLM

Boring Crew: DAIGNEAULT, HALL
Date Started: 9/04/13 Date Finished: 9/04/13
VTSPG NAD83: N 720677.02 ft E 1480342.49 ft
Station: 98+91.32 Offset: 30.20
Ground Elevation: 355.22 ft

Casing: WB Sampler: SS
Type: WB I.D.: 4 in 1.5 in
Hammer Wt: N.A. 140 lb.
Hammer/Rod: N.A. 30 in.
Hammer/Rod Type: Auto/AWJ
Rig: CME 45C TRACK $C_e = 1.34$

Groundwater Observations

| Date | Depth (ft) | Notes |
|----------|------------|-----------------|
| 09/04/13 | 1.6 | While drilling. |
| 09/04/13 | 0.0 | After drilling. |

| Depth (ft) | Strata (1) | CLASSIFICATION OF MATERIALS (Description) | Blows/6" (N Value) | Moisture Content % | Gravel % | Sand % | Fines % | LL % | PI % |
|------------|------------|---|----------------------|--------------------|----------|--------|---------|------|------|
| | | | | | | | | | |
| | | A-6, SiCl, brn, Moist, Rec. = 1.1 ft | WH-WH-2-2 (2) | 20.8 | 4.0 | 31.7 | 64.3 | 34 | 15 |
| | | A-2-4, SiSa, brn, Wet, Rec. = 0.4 ft | 4-4-7-12 (11) | 31.7 | 5.3 | 70.8 | 23.9 | 43 | 21 |
| | | A-7-6, Cl, brn, Moist, Rec. = 1.6 ft | | 24.2 | 0.4 | 9.1 | 90.5 | 43 | 21 |
| 5 | | A-7-6, Cl, brn, Moist, Rec. = 1.8 ft | 1-7-8-10 (15) | 26.2 | 0.9 | 7.2 | 91.9 | 44 | 21 |
| | | A-7-6, Cl, brn, Moist, Rec. = 1.8 ft | 2-8-9-12 (17) | 24.8 | 2.2 | 6.0 | 91.8 | 48 | 26 |
| | | A-7-6, Cl, gry, Moist, Rec. = 1.9 ft | 1-3-4-3 (7) | 33.1 | 0.8 | 1.3 | 97.9 | 49 | 26 |
| 10 | | GrCl, gry, Moist, Rec. = 0.9 ft, 10.0 ft - 10.9 ft, Shelby Tube | | | | | | | |
| | | Field Note:., Clean out with Roller Cone | | | | | | | |
| 15 | | Field Note:., Till, HP. No Recovery | 31-32-30-R@1.0" (62) | | | | | | |
| | | Field Note:., Clean out with Roller Cone | | | | | | | |
| 20 | | Field Note:., Till, HP. No Recovery | R@5.0" (R) | | | | | | |
| | | Field Note:., Clean out with Roller Cone | | | | | | | |
| 25 | | A-4, GrSaSi, gry, Moist, Rec. = 0.7 ft, R@25.9 ft. | (R) | 9.0 | 21.1 | 29.1 | 49.8 | | |
| | | Hole stopped @ 25.9 ft | | | | | | | |
| | | Remarks: 1. Hole collapsed at 20.2 ft. | | | | | | | |

BORING LOG 2 WILLISTON STP HES5500(12).GPJ VERMONT AOT.GDT 10/29/13

Notes: 1. Stratification lines represent approximate boundary between material types. Transition may be gradual.
2. N Values have not been corrected for hammer energy. C_e is the hammer energy correction factor.
3. Water level readings have been made at times and under conditions stated. Fluctuations may occur due to other factors than those present at the time measurements were made.



STATE OF VERMONT
 AGENCY OF TRANSPORTATION
 MATERIALS & RESEARCH SECTION
 SUBSURFACE INFORMATION

BORING LOG

WILLISTON
STP-HES 5500(12)
VT-2A ROADWAY

Boring No.: **B-102A**

Page No.: 1 of 1

Pin No.: 12D196

Checked By: MLM

Boring Crew: DAIGNEAULT, GARROW
 Date Started: 10/10/13 Date Finished: 10/10/13
 VTSPG NAD83: N 720676.77 ft E 1480343.29 ft
 Station: 98+91.30 Offset: 31.00
 Ground Elevation: 355.22 ft

Casing WB Sampler TUBE
 Type: WB TUBE
 I.D.: 4.25 in 3 in
 Hammer Wt: N.A. 140 lb.
 Hammer Fall: N.A. 30 in.
 Hammer/Rod Type: Auto/AWJ
 Rig: CME 55 TRACK C_E = 1.46

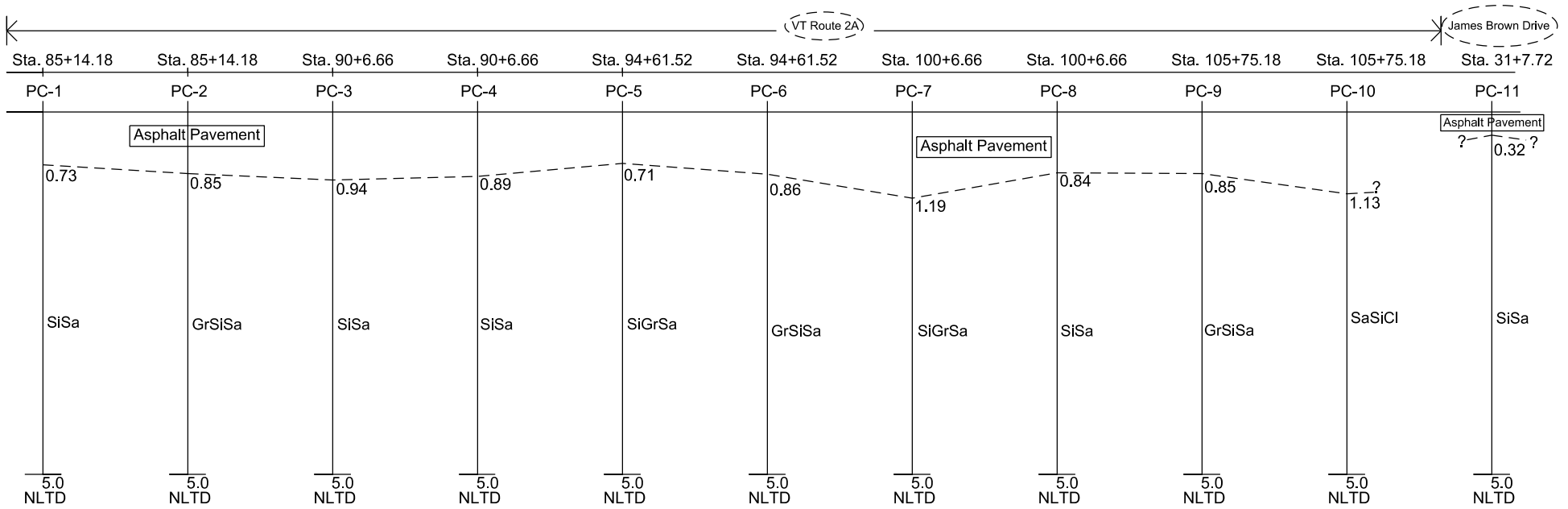
| Groundwater Observations | | |
|--------------------------|------------|-----------------|
| Date | Depth (ft) | Notes |
| 10/10/13 | 0.5 | While drilling. |
| | | |
| | | |

| Depth (ft) | Strata (1) | CLASSIFICATION OF MATERIALS (Description) | Blows/6" (N Value) | Moisture Content % | Gravel % | Sand % | Fines % |
|------------|------------|---|--------------------|--------------------|----------|--------|---------|
| 2.5 | | Field Note:., Cl, gry, Rec. = 0.5 ft, Shelby Tube | | | | | |
| 5.0 | | Field Note:., Vane Shear 1072 psf/Remold unsuccessful | | | | | |
| 7.5 | | Field Note:., Cl, gry, Rec. = 1.8 ft, Shelby Tube | | | | | |
| 10.0 | | Field Note:., Vane Shear 1334/459 psf | | | | | |
| 12.5 | | Hole stopped @ 10.5 ft | | | | | |
| 15.0 | | Remarks: 1. Vane used was 3x6 inches. 2. Vane Shear = Inital/Remold | | | | | |
| 17.5 | | | | | | | |

BORING LOG 2 WILLISTON STP-HES5500(12).GPJ VERMONT AOT.GDT 11/1/13

Notes: 1. Stratification lines represent approximate boundary between material types. Transition may be gradual.
 2. N Values have not been corrected for hammer energy. C_e is the hammer energy correction factor.
 3. Water level readings have been made at times and under conditions stated. Fluctuations may occur due to other factors than those present at the time measurements were made.

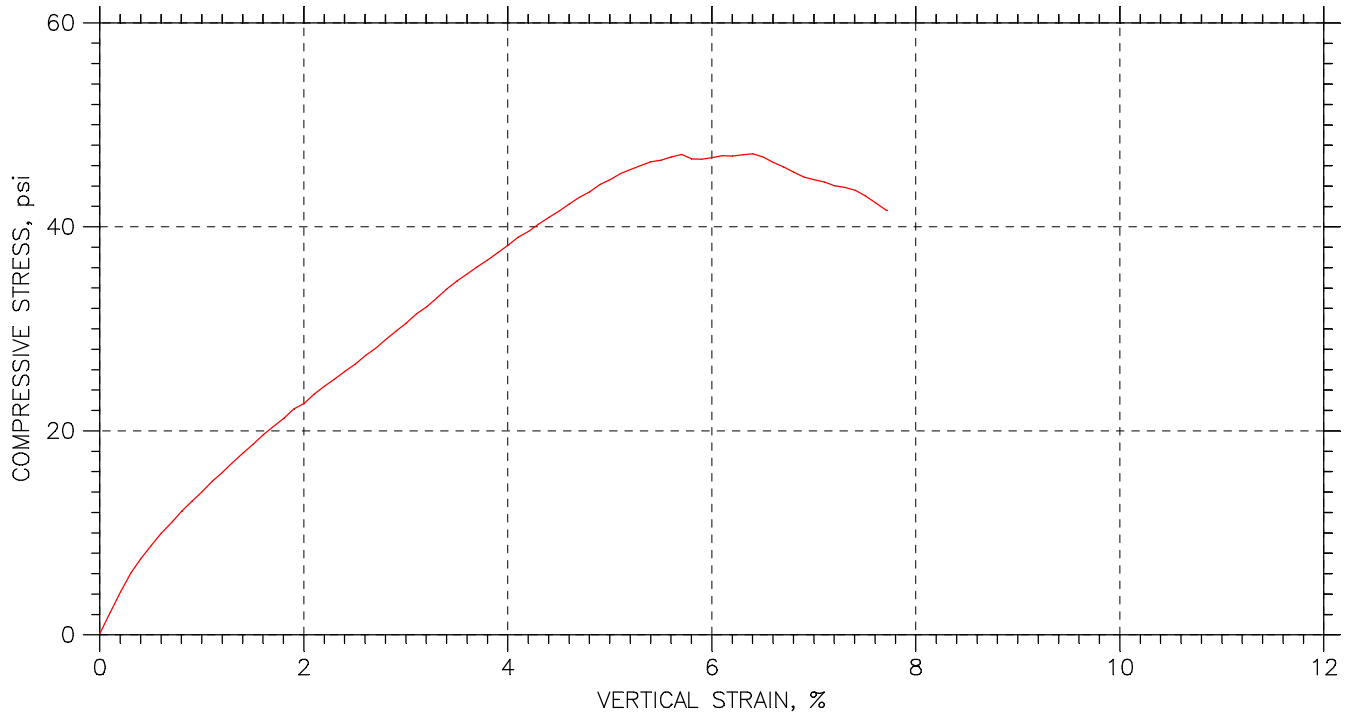
Williston STP HES 5500(12) -Auger Borings-



NOTES:
NLTD - No ledge to depth.

1. Vertical depths in feet.
2. Not to horizontal scale.
3. Groundwater was not encountered during drilling.

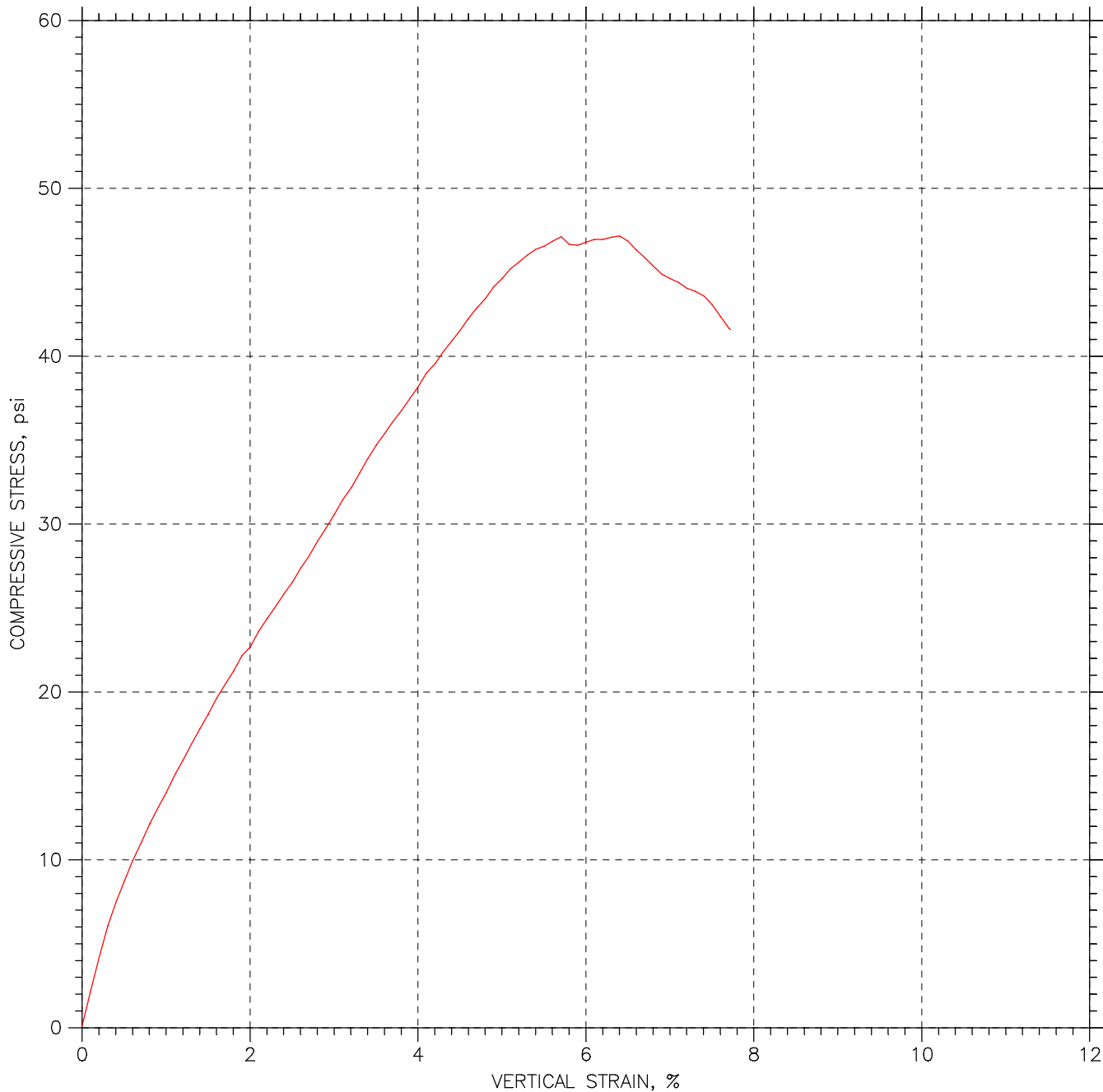
UNCONFINED COMPRESSION TEST REPORT



| | | | | |
|--------------------------------------|------------------|--------|--|--|
| Symbol | | | | |
| Test No. | | A | | |
| Initial | Diameter, in | 2.889 | | |
| | Height, in | 5.66 | | |
| | Water Content, % | 0.00 | | |
| | Dry Density, pcf | 123.7 | | |
| | Saturation, % | 0.00 | | |
| | Void Ratio | 0.337 | | |
| Unconfined Compressive Strength, psi | | 47.16 | | |
| Undrained Shear Strength, psi | | 23.58 | | |
| Time to Failure, min | | 6.1816 | | |
| Strain Rate, %/min | | 1 | | |
| Measured Specific Gravity | | 2.65 | | |
| Liquid Limit | | 0 | | |
| Plastic Limit | | 0 | | |
| Plasticity Index | | 0 | | |
| Failure Sketch | | | | |

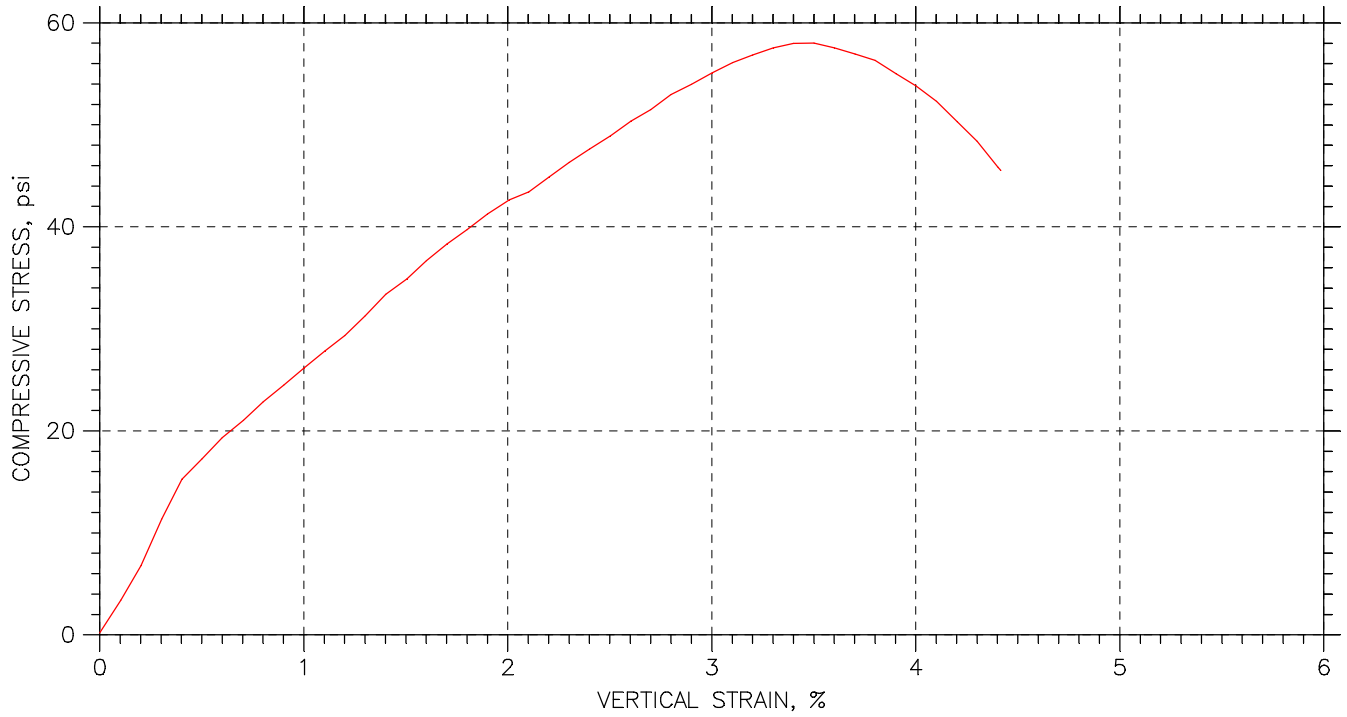
| | |
|--|-----------------------------|
| | Project: Williston |
| | Location: Williston, VT |
| | Project No.: 5500(12) |
| | Boring No.: B-102A |
| | Sample Type: Undisturbed |
| | Description: 2" into sample |
| | Remarks: |

UNCONFINED COMPRESSION TEST REPORT



| | | | |
|--|-----------------------------|--------------------------|-----------------------|
| | Project: Williston | Location: Williston, VT | Project No.: 5500(12) |
| | Boring No.: B-102A | Tested By: MLM/CEE | Checked By: |
| | Sample No.: U2 | Test Date: 10/16/13 | Depth: 7-9 feet |
| | Test No.: A | Sample Type: Undisturbed | Elevation: |
| | Description: 2" into sample | | |
| | Remarks: | | |
| | | | |

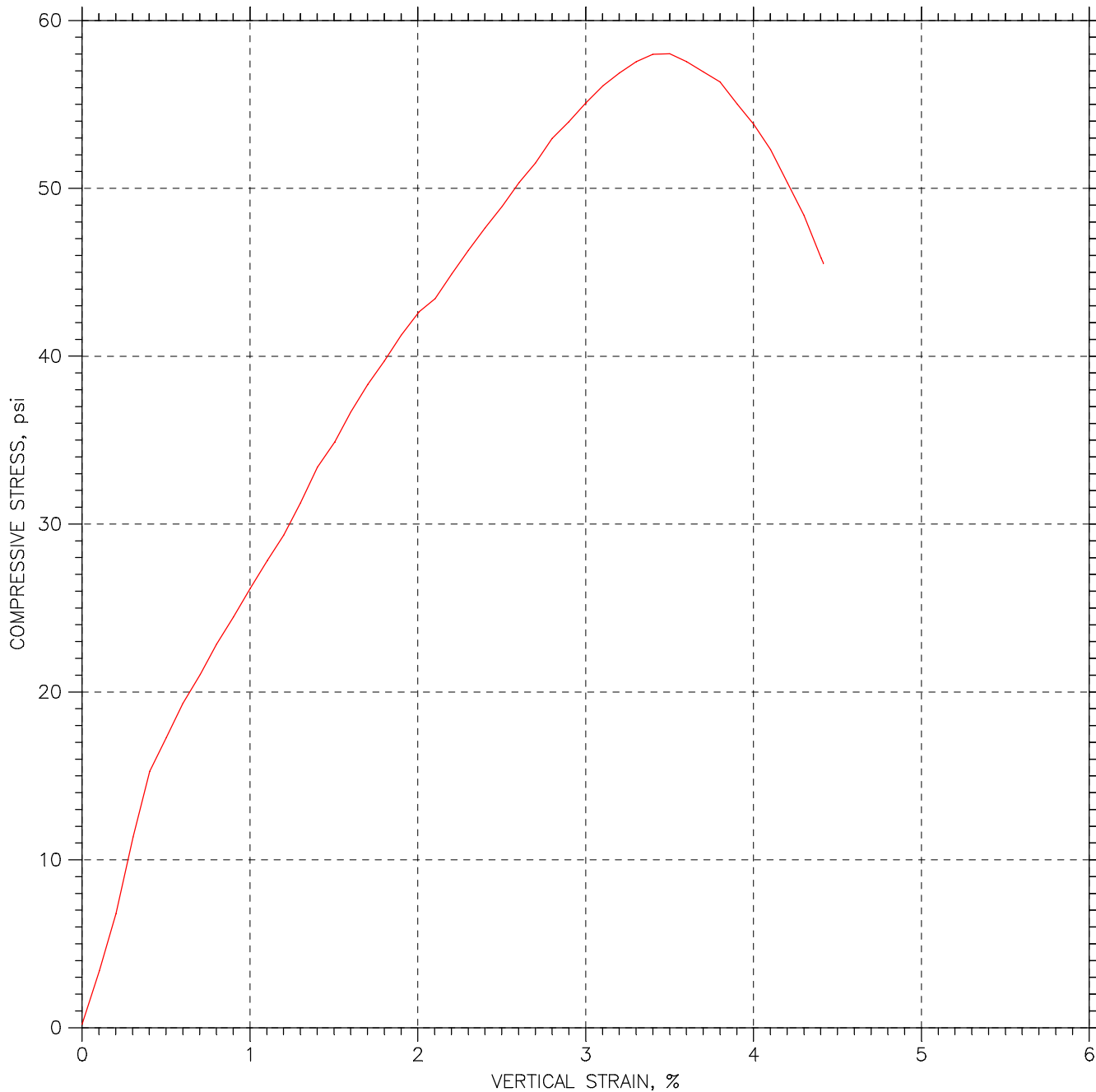
UNCONFINED COMPRESSION TEST REPORT



| | | | | |
|--------------------------------------|------------------|--------|--|--|
| Symbol | | | | |
| Test No. | | B | | |
| Initial | Diameter, in | 2.888 | | |
| | Height, in | 5.66 | | |
| | Water Content, % | 0.00 | | |
| | Dry Density, pcf | 122. | | |
| | Saturation, % | 0.00 | | |
| | Void Ratio | 0.356 | | |
| Unconfined Compressive Strength, psi | | 58.01 | | |
| Undrained Shear Strength, psi | | 29.01 | | |
| Time to Failure, min | | 3.3332 | | |
| Strain Rate, %/min | | 1 | | |
| Measured Specific Gravity | | 2.65 | | |
| Liquid Limit | | 0 | | |
| Plastic Limit | | 0 | | |
| Plasticity Index | | 0 | | |
| Failure Sketch | | | | |

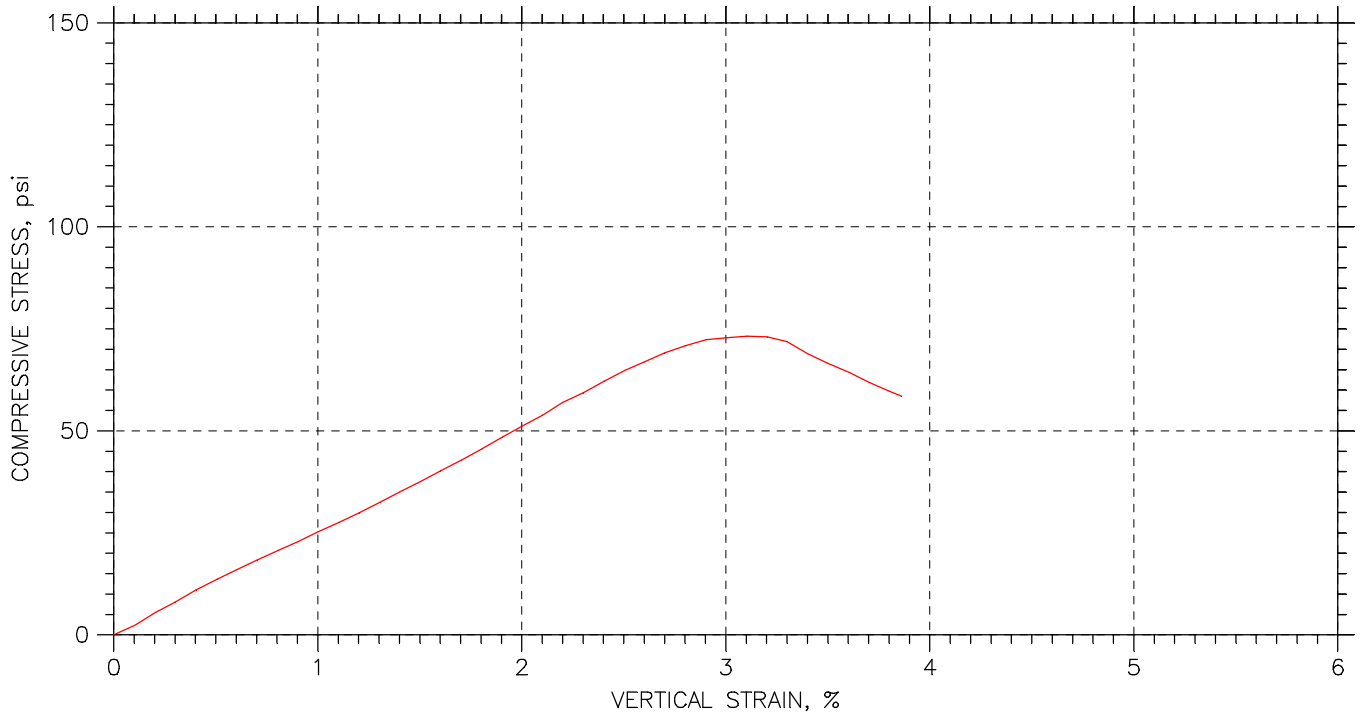
| | |
|--|-----------------------------|
| | Project: Williston |
| | Location: Williston, VT |
| | Project No.: 5500(12) |
| | Boring No.: B-102A |
| | Sample Type: Undisturbed |
| | Description: 8" into sample |
| | Remarks: |

UNCONFINED COMPRESSION TEST REPORT



| | | | |
|--|-----------------------------|--------------------------|-----------------------|
| | Project: Williston | Location: Williston, VT | Project No.: 5500(12) |
| | Boring No.: B-102A | Tested By: MLM | Checked By: |
| | Sample No.: U2 | Test Date: 10/17/13 | Depth: 7-9 feet |
| | Test No.: B | Sample Type: Undisturbed | Elevation: |
| | Description: 8" into sample | | |
| | Remarks: | | |
| | | | |

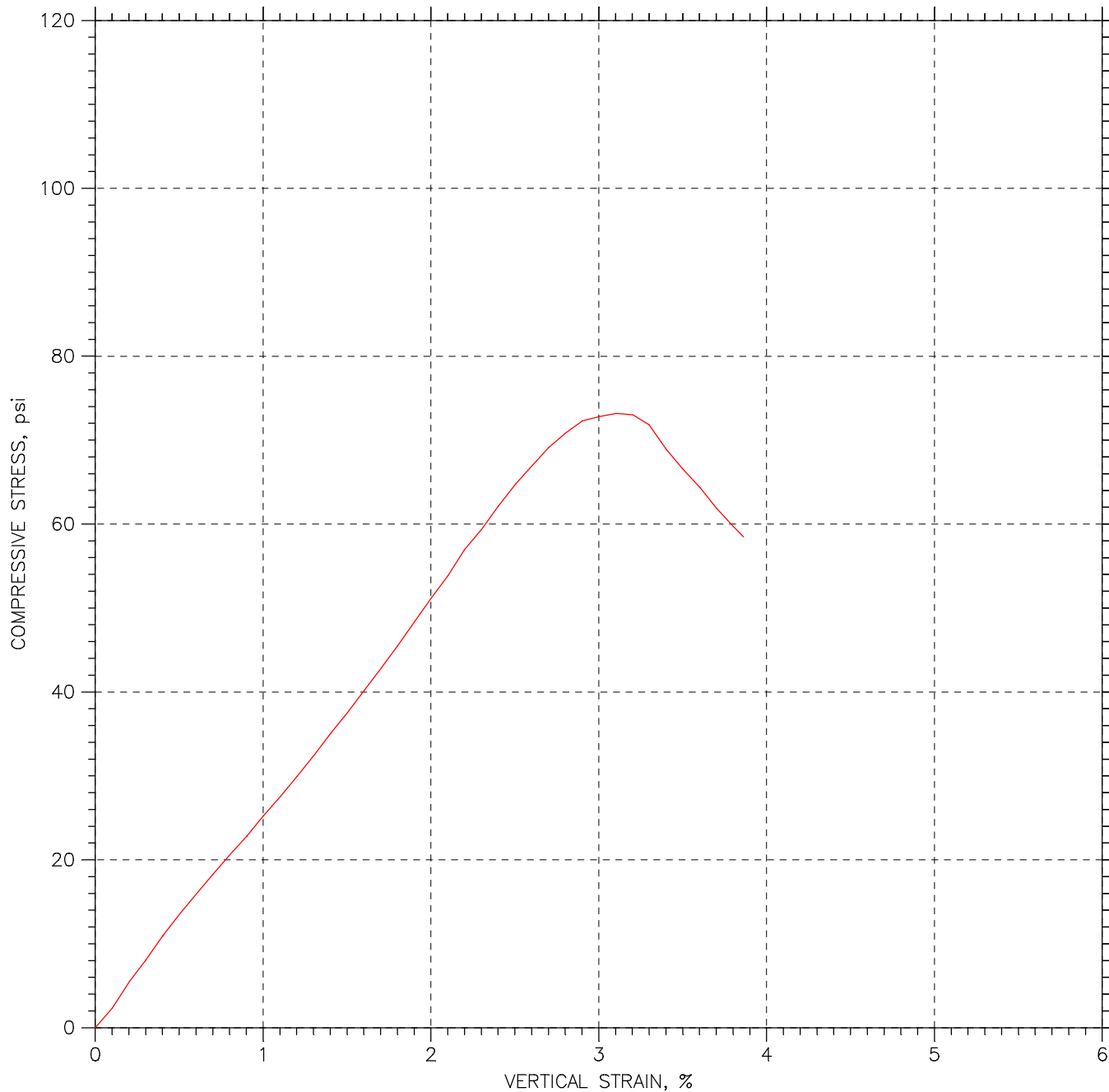
UNCONFINED COMPRESSION TEST REPORT



| | | | | |
|--------------------------------------|------------------|--------|--|--|
| Symbol | | | | |
| Test No. | | C | | |
| Initial | Diameter, in | 2.882 | | |
| | Height, in | 5.74 | | |
| | Water Content, % | 0.00 | | |
| | Dry Density, pcf | 124.1 | | |
| | Saturation, % | 0.00 | | |
| | Void Ratio | 0.333 | | |
| Unconfined Compressive Strength, psi | | 73.18 | | |
| Undrained Shear Strength, psi | | 36.59 | | |
| Time to Failure, min | | 3.0459 | | |
| Strain Rate, %/min | | 1 | | |
| Measured Specific Gravity | | 2.65 | | |
| Liquid Limit | | 0 | | |
| Plastic Limit | | 0 | | |
| Plasticity Index | | 0 | | |
| Failure Sketch | | | | |

| | |
|--|------------------------------|
| | Project: Williston |
| | Location: Williston, VT |
| | Project No.: 5500(12) |
| | Boring No.: B-102A |
| | Sample Type: Undisturbed |
| | Description: 14" into sample |
| | Remarks: |

UNCONFINED COMPRESSION TEST REPORT



| | | | |
|--|------------------------------|--------------------------|-----------------------|
| | Project: Williston | Location: Williston, VT | Project No.: 5500(12) |
| | Boring No.: B-102A | Tested By: MLM | Checked By: |
| | Sample No.: U2 | Test Date: 10/17/13 | Depth: 7-9 feet |
| | Test No.: C | Sample Type: Undisturbed | Elevation: |
| | Description: 14" into sample | | |
| | Remarks: | | |
| | | | |